Electron power absorption dynamics in capacitive radio frequency discharges driven by tailored voltage waveforms in CF$_4$

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Abstract

The power absorption dynamics of electrons and the electrical asymmetry effect in capacitive radio-frequency plasmas operated in CF$_4$ and driven by tailored voltage waveforms are investigated experimentally in combination with kinetic simulations. The driving voltage waveforms are generated as a superposition of multiple consecutive harmonics of the fundamental frequency of 13.56 MHz. Peaks/valleys and sawtooth waveforms are used to study the effects of amplitude and slope asymmetries of the driving voltage waveform on the electron dynamics and the generation of a DC self-bias in an electronegative plasma at different pressures. Compared to electropositive discharges, we observe strongly different effects and unique power absorption dynamics. At high pressures and high electronegativities, the discharge is found to operate in the drift-ambipolar (DA) heating mode. A dominant excitation/ionization maximum is observed during sheath collapse at the edge of the sheath which collapses fastest. High negative-ion densities are observed inside this sheath region, while electrons are confined for part of the RF period in a potential well formed by the ambipolar electric field at this sheath edge and the collapsed (floating potential) sheath at the electrode. For specific driving voltage waveforms, the plasma becomes divided spatially into two different halves of strongly different electronegativity. This asymmetry can be reversed electrically by inverting the driving waveform. For sawtooth waveforms, the discharge asymmetry and the sign of the DC self-bias are found to reverse as the pressure is increased, due to a transition of the electron heating mode from the $\alpha$-mode to the DA-mode. These effects are interpreted with the aid of the simulation results.

Keywords: voltage waveform tailoring, multi-frequency capacitive discharges, electronegative plasmas, electrical asymmetry effect

(Some figures may appear in colour only in the online journal)
1. Introduction

Optimal utilization of technological plasmas, such as those used in plasma medicine [1–3] or the plasma etching of semiconductors [4, 5], often requires finely tuned local plasma parameters, such as ion fluxes and particle energy distributions at a substrate surface. Customized flux-energy distribution functions for electrons, ions, and neutral radicals in these plasmas are necessary for optimum process control for a variety of applications such as anisotropic dielectric etching, plasma-enhanced chemical vapor deposition (PECVD) [6], etc. Such control is not possible in classical single-frequency capacitively coupled plasmas (CCPs) or single-source inductively coupled plasmas (ICPs) [7–11]. Classical dual-frequency CCPs operated at significantly different frequencies allow for separate control of ‘integral quantities’ of ion energy distribution functions (IEDFs) such as the mean ion energy and ion flux, but only within a certain window of operating conditions [11–16]. The addition of RF substrate biasing in ICPs allows the average ion energy to be increased in a controlled way.

A promising new way to achieve an advanced control of distribution functions and to improve the plasma’s lateral uniformity across large substrates is driving RF plasmas with tailored voltage waveforms [17–52]. With this technique, the sheath voltage waveforms as well as the time dependence of the electric field in the sheaths and in the plasma bulk can be customized on a nanosecond timescale. As a consequence, the ion and electron power absorption dynamics can be controlled and distribution functions of different particle species can be customized [17–20, 23–34, 37–39]. Integral quantities, such as the mean ion energies, can then be tailored for various applications. Recently, it was found that even the shape of the IEDF can be controlled using voltage waveform tailoring (VWT) [35, 36]. Johnson et al and Schüngel et al demonstrated various advantages of using VWT for PECVD [42–45].

Such voltage waveforms can be generated as a superposition consisting of multiple consecutive harmonics of a fundamental driving frequency. These waveforms can be customized by individually adjusting their harmonics’ amplitudes and phases. Any driving voltage waveform can be generated in this way using a sufficient number of harmonics. Efficient delivery of such waveforms with impedance matching is possible based on a novel RF supply and matching system [47].

Investigating the effect of the driving voltage waveform on the electron power absorption dynamics (referred to as electron heating dynamics in previous works [25–32, 39, 53–57]) is a crucial step in the fundamental understanding of the way these plasmas are generated. This is the basis for customizing distribution functions of both electrons and ions and, thus, for process optimization based on plasma science. A major stride towards this goal has been the discovery of the electrical asymmetry effect (EAE) in CCPs driven by two successive harmonics by Heil et al [17]. The EAE includes two effects: the amplitude asymmetry effect (AAE) and the slope asymmetry effect (SAE). The AAE is the generation of a DC self-bias as a function of the phase between the driving harmonics that changes the difference between the global extrema of the driving voltage waveform. The AAE was verified by simulations [18, 20, 22–24, 41] and experiments [19–24, 40, 46], as well as demonstrated to be strongly enhanced by using more than two harmonics [25–34, 37–39, 47, 48]. Later, Bruneau et al discovered the slope asymmetry effect (SAE) in argon, which also generates a DC self-bias and induces a discharge asymmetry by using sawtooth-like waveforms with identical global extrema, but with significantly different rise- and fall-times [49–52]. These previous investigations were mostly limited to electropositive plasmas operated in the α-heating mode.

An analytical model of the EAE introduced by Heil et al [17] has been described in detail by Czarnetzki et al [20]. Based on the individual voltage drops across the sheaths adjacent to each electrode and across the bulk, an expression for the DC self-bias, \( \eta \), is obtained in this model as [17, 20]:

\[
\eta = - \frac{\phi_{b_{\text{max}}}^f + \varepsilon \phi_{b_{\text{min}}}^f}{1 + \varepsilon} + \frac{\phi_{b_{\text{max}}}^b + \varepsilon \phi_{b_{\text{min}}}^b}{1 + \varepsilon},
\]

where \( \phi_{b_{\text{max}}}^f \) and \( \phi_{b_{\text{min}}}^f \) are the global maximum and minimum of the applied voltage waveforms, \( \phi_{b_{\text{max}}}^b \) and \( \phi_{b_{\text{min}}}^b \) are the floating potentials at the powered and grounded electrodes, and \( \phi_{b_{\text{max}}} \) and \( \phi_{b_{\text{min}}} \) are the voltage drops across the bulk at the times of maximum and minimum applied voltage, respectively. The bulk voltage drop \( \phi_b \) in equation (1) can usually be neglected for electropositive plasmas (e.g. argon) at low pressures [58], but cannot be neglected in the case of electronegative gases (e.g. CF) where significant drift electric fields are often present in the plasma bulk and ambipolar fields can be generated near the sheath edges [40, 41, 53, 59–64]. However, even for electronegative plasmas, the applied voltage waveform, i.e. the first term in equation (1) is typically dominant compared to the other terms. The symmetry parameter \( \varepsilon \) is defined by:

\[
\varepsilon = \left| \frac{\phi_{b_{\text{max}}}^f - \phi_{b_{\text{min}}}^f}{\phi_{b_{\text{max}}}^f + \phi_{b_{\text{min}}}^f} \right| \approx \left( \frac{A_p}{A_g} \right)^2 \left( \frac{Q_{\text{sp}}}{Q_{\text{sg}}} \right)^2 \left( \frac{I_g}{I_p} \right),
\]

with \( \phi_{b_{\text{max}}}^f \) and \( \phi_{b_{\text{min}}}^f \) being the maximum voltage drops across each sheath (note that \( \phi_{b_{\text{max}}}^f < 0 \) V and \( \phi_{b_{\text{min}}}^f > 0 \) V). The variables on the right hand side of equation (2) correspond to the respective electrode surface areas \( A_p \) and \( A_g \), the respective mean charge densities in each sheath \( n_{sp} \) and \( n_{sg} \), the maximum uncompensated charges in each sheath \( Q_{\text{sp}} \) and \( Q_{\text{sg}} \), and the sheath integrals for each sheath \( I_{sp} \) and \( I_{sg} \) (for details see [17, 20, 58]). The symmetry parameter \( \varepsilon \) compares the plasma conditions at each sheath to determine the influence on the DC self-bias due to any spatial asymmetry (from different effective electrode surface areas), or from plasma sheath parameters, which affect the generation of a DC self-bias (\( \eta \)). The effect of the difference between the driving voltage waveform’s global extrema on both the symmetry parameter and the DC self-bias can thus be referred to as the amplitude asymmetry effect (AAE). By using two or more consecutive harmonics of a fundamental frequency with distinct phases, \( \phi_{b_{\text{max}}}^f \) and \( \phi_{b_{\text{min}}}^f \) can be made unequal.
The slope asymmetry effect (SAE) is described in detail in the works of Bruneau et al. [49–52]. Qualitatively, the SAE is the result of a temporal asymmetry in the positive (rise) and negative (fall) slopes of the applied voltage waveform. As the applied voltage waveform determines the (differing) voltage drops across each individual sheath, this leads to drastically different sheath dynamics, with a quickly expanding sheath at one electrode and a slowly expanding sheath at the opposing electrode. For electropositive discharges operated in the $\alpha$-heating mode, the ‘fast’ expanding sheath accelerates electrons and (at high pressures) induces ionization locally near the given electrode, leading to a higher local ion density compared to the other electrode [49–52] and inducing an electrical asymmetry ($\varepsilon \neq 1$), as indicated by equation (2). The SAE may also affect other parameters associated with $\varepsilon$ such as the sheath integrals [17, 20, 58].

The influence of the SAE on the electron power absorption and ionization dynamics will strongly depend on the electron heating mode, which in turn depends on pressure, driving frequency, and the relative phases between harmonics [25–34, 37–39, 41, 49–57, 59–61, 63–78]. In contrast to low pressure electropositive discharges ($\alpha$-mode), a different heating mode caused by a significant electric field in the plasma bulk, known as the drift-ambipolar mode, has been observed in electronegative gases [40, 59, 61, 63, 66, 75, 79]. Under these conditions, electrons are accelerated towards the electrode during sheath collapse by a drift electric field in the plasma bulk and by ambipolar fields at the sheath edges. The drift electric field is a consequence of the reduced bulk conductivity, which itself is a result of the reduced electron density due to the attachment of electrons to the gas molecules, forming negative ions with low mobility. These negative ions are confined within the bulk plasma and do not generally reach the electrodes. The ambipolar field is the consequence of the peaked electron density at the sheath edges, which create strong density gradients towards the bulk [40, 59, 78]. Significant electron acceleration occurs in the bulk for this heating mode, and strong local field reversals which also cause electron energy gain can be observed at the collapsing sheath edge [68–70, 79, 80]. If this heating during sheath collapse (field reversal heating) is dominant, the SAE will cause the discharge symmetry to be reversed compared to discharges operated in the $\alpha$-mode [52].

Previous fundamental studies on the effects of voltage waveform tailoring on the electron power absorption and excitation/ionization dynamics have been mostly restricted to electropositive argon discharges operated in the $\alpha$-mode [25–32, 39, 53–57]. The fundamental knowledge of these dynamics is incomplete for process relevant electronegative and reactive gases (e.g. CF$_4$, which is often used in processing applications), where different electron heating modes are dominant. The effects of different gas chemistries on the electron power absorption dynamics and the generation of a DC self-bias in RF discharges driven by tailored voltage waveforms are inadequately understood.

Here, we present the first systematic experimental investigation of the electron power absorption dynamics and the EAE in CCPs driven by tailored voltage waveforms operated in CF$_4$, where the drift-ambipolar heating mode is prevalent. Experimental measurements of the DC self-bias and phase-resolved optical emission spectroscopy (PROES) are combined with particle-in-cell (PIC) simulations to obtain a complete understanding of the electron power absorption dynamics. We investigate the effects of the gas pressure, the harmonics’ phases, and the number of harmonics under the conditions of both the amplitude and slope asymmetry effects.

We show that, due to the presence of the drift-ambipolar electron heating mode [40, 59, 61, 63, 66, 75, 79], the effect of VWT on the electron power absorption and excitation dynamics in CF$_4$ can differ significantly from those in electropositive discharges. Mode transitions are observed as a function of pressure and harmonics’ phases. These transitions drastically affect the discharge symmetry and heating dynamics. For specific harmonic phases, it is found that the discharge can be split into a strongly electronegative half and an electropositive (or weakly electronegative) half. In the strongly electronegative half, a high negative-ion density occurs close to one electrode. This unique structure is caused by a comparatively long time of sheath collapse, a strong ionization source adjacent to the electrode, and the creation of a potential well. Electrons are confined in this well and efficiently generate negative ions locally via dissociative attachment. These dynamics are induced by particular shapes of the driving voltage waveform and are expected to provide unique advantages for a variety of applications.

This paper is structured in the following way: in section 2, the experimental setup and all diagnostic methods are introduced. The PIC/MCC code used in the numerical studies is briefly described in section 3. The presentation of the results in section 4 is divided into two parts. First, systematic phase variations using different numbers of driving frequencies, i.e. voltage waveform tailoring, are performed at different pressures. Waveforms with specific sets of phases between harmonics are then used to study either the AAE or a non-optimized SAE. Second, sawtooth waveforms are studied as one important waveform shape at different pressures. From these studies, the slope asymmetry effect is enhanced and isolated from the amplitude asymmetry effect, since the absolute values of the global extrema for sawtooth waveforms are identical. In both parts, the formation of a DC self-bias and the spatio-temporal excitation dynamics are analyzed and understood based on the experimental and computational results. Finally, conclusions are drawn in section 5.

2. Experimental setup

2.1. Reactor and diagnostics

The experimental setup is shown in figure 1. The capacitively coupled plasma is operated inside a modified gaseous electronics conference (GEC) reference cell by applying specific multi-frequency voltage waveforms to the powered (bottom) electrode while keeping the other (top) electrode and the chamber walls grounded. Up to three consecutive harmonics of the fundamental frequency $f = 13.56$ MHz are applied to the system. The harmonics’ amplitudes and relative phases are tuned in order to realize the prescribed voltage waveforms.
A novel RF power supply system and impedance matching are used to generate these waveforms [47]. The system consists of three RF signal generators, each outputting a single frequency corresponding to one of the first three harmonics of the fundamental frequency, i.e. $f_1 = 13.56$ MHz, $f_2 = 27.12$ MHz, and $f_3 = 40.68$ MHz. These signals are phase-locked by a control unit and each generator’s signal is matched individually before being combined at the powered electrode to drive the RF plasma. Electrical filters in each matching network prevent parasitic interactions between the signal branches [47].

The discharge is operated in CF$_4$ at pressures between 10 Pa and 100 Pa inside a 25 mm gap between two circular, stainless steel electrodes having a diameter of 10 cm. The plasma is radially confined between the electrodes by a glass cylinder. The discharge is slightly geometrically asymmetric due to capacitive coupling between the glass cylinder and the grounded side walls of the vacuum chamber [19, 81, 82]. This capacitive coupling effectively increases the grounded electrode area, which results in a small geometric asymmetry even though the material areas of each electrode are the same (see equation (2)) [81, 82]. Therefore, a negative DC self-bias is present even for single-frequency sinusoidal waveforms. At high pressures, the capacitive coupling between the cylinder and the walls has a weaker effect. The importance of the capacitive coupling between the cylinder and the grounded walls decreases because of the higher plasma density at high pressures, which increases the current flowing through the plasma and reduces the significance of the current flowing as a displacement current to the walls. The symmetry is significantly better at such higher pressures, and thus only the results at higher pressure will be compared with the results of the simulations, which assume perfect geometrical symmetry.

The plasma is investigated experimentally by utilizing two diagnostics: a high voltage probe and an ICCD (intensified charge-coupled device) camera used for PROES. The high voltage probe is attached to the coaxial cable connecting the combined frequency branches and the powered electrode (see figure 1) and allows measurements of the applied voltage waveform using an oscilloscope. The amplitudes and phases of the three consecutive harmonics of the voltage waveform are determined at the powered electrode’s surface via Fourier analysis and a calibration routine previously used in dual- and triple-frequency discharges [19, 47]. This calibration procedure is performed by venting the chamber and attaching the high voltage probe to the powered electrode’s surface. Comparisons of the voltage waveform parameters (harmonic amplitudes, phases) at the measurement point on the coaxial cable and at the electrode surface yield calibration factors for each harmonic’s amplitude and phase. These calibration factors are strongly system dependent and are different for each applied frequency. This calibration procedure relies on the assumption that the impedance of the plasma is similar to the impedance when the chamber is vented, which is usually valid for CCPs due to their low plasma densities compared with inductively coupled plasmas or hybrid setups [19]. The high voltage probe and oscilloscope are used to tune the voltage waveform parameters as necessary to achieve the desired waveform.

In order to perform phase-resolved optical emission spectroscopy (PROES), an ICCD camera with an optical filter is placed outside a GEC cell viewport. PROES is a non-intrusive diagnostic that probes the dynamics of highly energetic electrons, which sustain the discharge through ionization, with high spatial and temporal resolutions within the RF period [66-68, 83-85]. Emission from a specifically chosen Fluorine transition at 703.7 nm with a lifetime of about 26.3 ns [86] is resolved in space and time by this nanosecond-gated, high repetition rate ICCD camera (Andor iStar) synchronized with the applied RF voltage waveform. A more complete description of PROES can be found in [83]. Analysis of PROES data via a simple collisional-radiative model [83] yields the experimental spatio-temporal excitation rate plots. These plots have a spatial resolution better than 1 mm and a temporal resolution of about 2 ns.

### 2.2. Driving voltage waveforms

Different types of voltage waveforms are used to drive the CCP. The ‘peaks’/‘valleys’ waveforms are applied to optimize the AAE (see figure 2(a)), while the sawtooth waveforms are used to optimize and study the SAE separately from the AAE (see figure 2(c)). Intermediate waveforms shown in figure 2(b) isolate the SAE from the AAE, but do not optimize the SAE. All waveforms are generated as a superposition of multiple consecutive harmonics [25-32, 39]:

$$\tilde{\phi}(t) = \sum_{k=1}^{N} \phi_k \cos(2\pi f_k t + \theta_k),$$

(3)

where $N$ is the total number of harmonics, $k$ is the harmonic index, $f = 13.56$ MHz is the fundamental frequency, $\phi_k$ are the harmonics’ amplitudes, and $\theta_k$ are the harmonics’ phases. The total possible amplitude of the waveform is $\phi_{\text{tot}} = \sum_{k=1}^{N} \phi_k$, but because of destructive interference between the harmonics, this amplitude is not reached for every set of phases. The phase of the first harmonic (13.56 MHz), i.e. $\theta_1$, is subtracted from all phases such that $\theta_k = 0$ for any waveform. Therefore, the other harmonics’ phases ($\theta_k, k \neq 1$) are relative to the phase of the fundamental 13.56 MHz component in equation (3).
‘Peaks’ waveforms are generated by setting all phases to zero ($\theta_2 = 0^\circ$), while $\theta_2 = 180^\circ$, $\theta_1 = \theta_3 = 0^\circ$ define the ‘Valleys’ waveforms. The intermediate waveforms shown in figure 2(b) are generated by choosing $\theta_1 = \theta_3 = 0^\circ$ and either $\theta_2 = 90^\circ$ or $\theta_2 = 270^\circ$. The harmonics’ amplitudes are chosen according to the following criterion [25]:

$$\phi_k = \phi_{\text{tot}} \frac{2(N - k + 1)}{N(N + 1)}.$$  \hspace{1cm} (4)

We set $\phi_{\text{tot}} = 210$ V. Dual- ($\phi_1 = 140$ V, $\phi_2 = 70$ V) and triple- ($\phi_1 = 105$ V, $\phi_2 = 70$ V, $\phi_3 = 35$ V) frequency cases are studied.

For sawtooth waveforms, the harmonic amplitudes are chosen according to the following criterion [49–52]:

$$\phi_k = \frac{\phi_N}{k},$$  \hspace{1cm} (5)

where $\phi_N$ changes with the total number of harmonics ($N$). Here we study the triple-frequency case ($N = 3$) with $\phi_N = 138$ V and thus $\phi_1 = 138$ V, $\phi_2 = 69$ V, and $\phi_3 = 46$ V. The resulting waveform oscillates between the peak values $\pm 200$ V. The total possible amplitude $\phi_{\text{tot}} = 253$ V was chosen so that the absolute possible positive and negative voltages were approximately the same as those reached by the AAE waveforms. For the sawtooth up waveform, the phases are set to $\theta_1 = 0^\circ$, $\theta_2 = 270^\circ$, and $\theta_3 = 180^\circ$. The sawtooth down waveform has phases $\theta_1 = 0^\circ$, $\theta_2 = 90^\circ$, and $\theta_3 = 180^\circ$. This choice of individual harmonic amplitudes and phases makes the slope of the slowly rising/falling part of the waveform more linear and the fast drop/rise steeper (see figure 2(c)), thus enhancing the SAE.

Historically, waveforms designed from the harmonics’ amplitudes criterion of equation (4) were used before the use of sawtooth waveforms and will therefore be called ‘classical tailored voltage waveforms’ in this work.

3. Simulations

Our numerical studies of CF$_4$ plasmas are based on a bounded 1D3V particle-in-cell simulation code, complemented with a Monte Carlo treatment of collision processes (PIC/MCC) [87–89]. The electrodes are assumed to be planar and parallel. To further simplify, the large aspect ratio (electrode diameter over electrode separation) of the experimental device justifies neglecting the radial losses. The discharge modeled by the code is assumed to be perfectly geometrically symmetric. The powered electrode is driven by the voltage waveforms specified in section 2.2, while the other electrode is grounded.

The charged species taken into account in the model are CF$_3^+$, CF$_2^-$, F$^-$ ions, and electrons. The cross-sections of electron-CF$_4$ collision processes (see table 1) are adopted from Kurihara et al [90], with the exception of electron attachment processes (producing CF$_3^-$ and F$^-$ ions), which are adopted from Bonham [91]. The electron-impact collision processes considered in the model are listed in table 1 and their energy dependent cross-sections are displayed in figure 3. As a simplification, the processes that create radicals, or charged species other than CF$_3^+$, CF$_2^-$, and F$^-$, are allowed to affect only the electron kinetics and the products are not otherwise accounted for.

Ion-molecule reactive reactions, as well as elastic collisions are also considered in the simulation [92–95]. For the elastic collisions of ions with buffer gas molecules, we adopt Langevin type cross-sections:
Table 1. List of electron-CF₄ molecule collision processes considered in the model.

<table>
<thead>
<tr>
<th>Collision partners</th>
<th>Description</th>
<th>Product</th>
<th>$E_0$</th>
</tr>
</thead>
<tbody>
<tr>
<td>e⁻ + CF₄</td>
<td>Elastic momentum transfer</td>
<td>0</td>
<td></td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Vibrational excitation</td>
<td>0.108</td>
<td></td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Vibrational excitation</td>
<td>0.168</td>
<td></td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Electronic excitation</td>
<td>0.077</td>
<td></td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Dissociative ionization</td>
<td>CF⁺₄</td>
<td>7.54</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Dissociative ionization</td>
<td>CF⁺</td>
<td>41</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Dissociative ionization</td>
<td>CF⁺</td>
<td>16</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Dissociative ionization</td>
<td>CF⁺</td>
<td>42</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Dissociative ionization</td>
<td>CF⁺</td>
<td>21</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Dissociative ionization</td>
<td>CF⁺</td>
<td>26</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Dissociative ionization</td>
<td>C⁺</td>
<td>34</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Dissociative ionization</td>
<td>F⁻</td>
<td>34</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Attachment</td>
<td>F⁻</td>
<td>0</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Attachment</td>
<td>CF⁺₃</td>
<td>0</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Neutral dissociation</td>
<td>CF⁺₂</td>
<td>12</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Neutral dissociation</td>
<td>CF⁺₂</td>
<td>17</td>
</tr>
<tr>
<td>e⁻ + CF₄</td>
<td>Neutral dissociation</td>
<td>CF⁺₂</td>
<td>18</td>
</tr>
</tbody>
</table>

Note: $E_0$ is the threshold energy in eV [90, 91].

Figure 3. Cross-sections of electron-impact collision processes [90, 91].

$$\sigma_{\text{el}} \equiv \left( \frac{\pi \alpha p e^2}{\epsilon_0 \mu} \right)^{1/2} \beta_{\infty} g^{-1},$$  \hspace{1cm} (6)

where $\mu$ is the reduced mass, $\alpha_p$ is the polarizability, $g$ is the relative velocity of the colliding partners, and $\beta_{\infty}$ is the dimensionless impact parameter for which the deflection angle is negligible [92–94]. The ion-molecule reaction processes considered in our model are listed in table 2 and their cross-sections are shown in figure 4.

The ion-molecule reactions produce the charged species considered in the model (CF⁺₃, CF⁺₄, F⁻, and e⁻), with the exception of the first reaction in table 2 that results in the formation of CF⁺₂ ions. CF⁺₃ and CF⁺₄ ions react similarly with CF₄ and the recombination rate of CF⁺₂ with electrons is only slighter higher than the recombination rate of CF⁺₃ [96]. We assume, as a simplification, that the above CF⁺₂ generation process does not convert CF⁺₃ ions to CF⁺₂ ions. This is further justified by the high rates for CF⁺-neutral and CF⁺₂-neutral reactions, which convert these lighter ions into CF⁺₂ ions [97]. This assumption makes it unnecessary to introduce an additional type of charged species of minor importance into the computations and improves the balance of positive ion density.

Recombination processes between positive and negative ions as well as between electrons and CF⁺₃ ions are simulated according to the procedure outlined in the work of Nanbu and Denph [98]. The ion–ion recombination rate coefficients are

Table 2. Ion-CF₄ molecule collision processes considered in the model.

<table>
<thead>
<tr>
<th>Projectile</th>
<th>Reaction</th>
<th>$E_0$</th>
</tr>
</thead>
<tbody>
<tr>
<td>CF⁺₃⁺</td>
<td>CF⁺₃⁺ + CF₄ → CF⁺₃ + CF₄ + F</td>
<td>5.843</td>
</tr>
<tr>
<td>CF⁺₃⁺</td>
<td>CF⁺₃⁺ + CF₄ → CF⁺₃ + CF₄ + F</td>
<td>5.621</td>
</tr>
<tr>
<td>CF⁺₃⁺</td>
<td>CF⁺₃⁺ + CF₄ → CF⁺₃ + CF₄</td>
<td>0</td>
</tr>
<tr>
<td>CF⁺₃⁺</td>
<td>CF⁺₃⁺ + CF₄ → CF⁺₃ + CF₄ + e⁻</td>
<td>1.871</td>
</tr>
<tr>
<td>CF⁺₃⁺</td>
<td>CF⁺₃⁺ + CF₄ → CF⁺₃ + CF₄ + e⁻</td>
<td>5.621</td>
</tr>
<tr>
<td>CF⁺₃⁺</td>
<td>CF⁺₃⁺ + CF₄ → CF⁺₃ + CF₄ + e⁻</td>
<td>1.927</td>
</tr>
<tr>
<td>CF⁺₃⁺</td>
<td>CF⁺₃⁺ + CF₄ → CF⁺₃ + CF₄</td>
<td>0</td>
</tr>
<tr>
<td>F⁻</td>
<td>F⁻ + CF₄ → F⁻ + CF₄ + F + e⁻</td>
<td>3.521</td>
</tr>
<tr>
<td>F⁻</td>
<td>F⁻ + CF₄ → F⁻ + CF₄ + F + e⁻</td>
<td>5.621</td>
</tr>
<tr>
<td>F⁻</td>
<td>F⁻ + CF₄ → F⁻ + CF₄</td>
<td>0</td>
</tr>
</tbody>
</table>

Note: $E_0$ is the threshold energy in eV [92–95].

Figure 4. Cross-sections of ion-impact collision processes [92–95].

Table 3. Recombination processes considered in the model.

<table>
<thead>
<tr>
<th>Reaction</th>
<th>Rate coefficient (m³·s⁻¹)</th>
</tr>
</thead>
<tbody>
<tr>
<td>CF⁺₃⁺ + e⁻</td>
<td>$3.95 \times 10^{-15} T_i^{-0.5} T_e^{-0.5}$</td>
</tr>
<tr>
<td>CF⁺₃⁺ + F⁻</td>
<td>$5.5 \times 10^{-13}$</td>
</tr>
<tr>
<td>CF⁺₃⁺ + CF⁺₃⁺</td>
<td>$5.5 \times 10^{-13}$</td>
</tr>
</tbody>
</table>

Note: The ion and electron temperatures, $T_i$ and $T_e$, respectively, are given in electronvolts [91, 98–100].
adopted from Proshina et al [99], while the rate for the electron-CF$_3$ recombination process is from Denpoh and Nanbu [100]. The recombination processes are listed in table 3.

In the simulations, we assume a gas temperature of 350 K. We include the emission of secondary electrons from the electrodes due to ion impact via the secondary electron emission coefficient, $\gamma$, which is set at $\gamma = 0.4$ for the best agreement with experimental results. In the experiment, the plasma is reactive and operates at a relatively high pressure. Consequently, a thin film with unknown properties is depos-ited on the electrode. This high secondary electron emission coefficient in the simulations is required to reproduce the experimentally measured DC self-bias. The excitation rate from energetic secondary electrons is smaller in CF$_3$ compared to Argon due to the lower positive ion flux in CF$_4$. The secondary electrons also cause more ionization than excitation due to their differing cross sections and can strongly affect the discharge symmetry via ionization in the sheaths. The (elastic) reflection of electrons from the electrodes is also considered; we adopt a reflection probability value of 0.2 [101].

For the specific driving voltage waveforms used here, a DC self-bias generally builds up on the powered electrode (which is capacitively coupled) in order to equalize the time-averaged electron and positive ion fluxes to each of the electrodes. Negative ions are confined within the bulk and do not reach the electrodes. This self-bias is adjusted in the simulation in an iterative way to satisfy the current (i.e. flux) balance requirement mentioned above.

The electron-impact excitation rate from ground-state F atoms to the excited F-level responsible for the 703.7 nm emission observed experimentally by PROES is approximated in the simulation using the cross-section for the electronic excitation process for CF$_4$ having a threshold of 7.54 eV (see figure 3 and table 1) by specifically accumulating excitation data for electrons with energies equal to or higher than 14.5 eV. This calculation is used exclusively for diagnostic purposes and does not affect the total electronic excitation calculated in the code. We further assume that the F atom density is uniform in space and does not vary over time. In this way, we compare the simulated spatio-temporal dynamics of electrons to the experimental PROES measurements without explicitly including F atoms in the simulation.

4. Results

This section is divided into two parts according to the different shapes of the driving voltage waveform used to operate the CCP. First, classical tailored voltage waveforms are used based on harmonics’ amplitudes chosen according to equation (4) and a systematic variation of $\theta_2$ ($\theta_1 = \theta_3 = 0^\circ$). Such waveforms generate a pure AAE (‘Peaks’/ ‘Valleys’ waveforms), or a non-optimized SAE ($\theta_2 = 90^\circ$, 270$^\circ$ waveforms). Second, sawtooth waveforms are used to isolate the SAE from the AAE, while also optimizing the SAE. The harmonics’ amplitudes are chosen according to equation (5) with $\theta_1 = 0^\circ$, $\theta_2 = 270^\circ$, $\theta_3 = 180^\circ$ for sawtooth up waveforms and $\theta_1 = 0^\circ$, $\theta_2 = 90^\circ$, $\theta_3 = 180^\circ$ for sawtooth down waveforms.

The effects of each voltage waveform on the spatio-temporal electron power absorption dynamics and the generation of a DC self-bias are studied by a synergistic combination of experiments and simulations to obtain a complete interpretation of the effect of using a reactive electronegative gas such as CF$_3$ on the EAE in CCPs driven by customized voltage waveforms.

4.1. Amplitude asymmetry

A driving voltage waveform according to equation (3), with amplitudes according to equation (4), is used. Single- ($N = 1$), dual- ($N = 2$), and triple- ($N = 3$) frequency scenarios are investigated. Here, $\phi_{tot} = 210$ V is kept constant while $\theta_2$ is varied. Two different pressures of 20 Pa and 80 Pa are used to study a weakly electronegative (20 Pa) and a strongly electronegative (80 Pa) scenario.

The measured and simulated DC self-bias voltages are shown in figure 5 as a function of the second harmonic’s phase (the 27 MHz signal’s phase, $\theta_2$) for both 80 Pa and 20 Pa. The other harmonics’ phases are fixed at zero throughout these variations. In the experiment, the discharge is always geometrically asymmetric at 20 Pa, as indicated by the $\eta \approx -29$ V value obtained for $N = 1$ (see figure 3(a)). Therefore, we do not compare the 20 Pa measurements to the results of the (geometrically symmetric) simulation. At 20 Pa, the control range of $\eta$ is increased by using more harmonics for the same total voltage, due to an enhanced amplitude asymmetry effect (AAE) similar to the AAE in electropositive argon discharges [19–24, 31, 32, 39]. For 80 Pa, the control range of $\eta$ is larger for $N = 2$ compared to $N = 3$ and the functional dependence of the bias on the phase is significantly different. This is caused by the presence of a different electron heating mode which enhances the slope asymmetry effect (SAE) for $N = 2$ at phases around 90$^\circ$ and 270$^\circ$. This heating mode will be discussed later in this section. The $N = 2$ DC self-bias caused by the SAE at $\theta_2 = 90^\circ$ is almost the same as the one caused by the AAE at $\theta_2 = 180^\circ$. Such an effect is not observed in the $N = 3$ case.

Figure 6 shows spatio-temporal plots of the different plasma parameters obtained from the experiment and the simulation, for $\theta_2 = 0^\circ$ and $N = 3$. Figures 6(a) and (b) show the spatio-temporal excitation rate and the electric field obtained from the simulation at 80 Pa, while figures 6(c) and (d) show the excitation rate obtained experimentally at 80 Pa and 20 Pa, respectively. In the experiment, the excitation at the (bottom) powered electrode is enhanced with respect to the maxima observed at the grounded electrode due to the geometric asymmetry of the reactor. This does not happen in the simulation and, therefore, the excitation rate at the powered electrode is stronger in the experiment compared to the simulation. Nevertheless, good qualitative agreement is found throughout. The asymmetry of the discharge drastically changes between 20 and 80 Pa as the excitation maximum near the powered electrode moves towards the grounded electrode at higher pressures as the result of a heating mode transition. At 20 Pa, $\alpha$-mode heating is dominant (see figure 6(d)), whereas drift-ambipolar mode heating is prevalent at 80 Pa (see figures 6(a)
Figure 5. DC self-bias as a function of $\theta_2$ for (a) 20 Pa (experimentally measured bias) and (b) 80 Pa (including both the experimentally measured bias and the bias obtained from the PIC simulation, a.k.a. ‘Sim.’) for different numbers of applied harmonics, $N = 1, 2, 3$. $\phi_{tot} = 210$ V for all cases.

Figure 6. Spatio-temporal plots for $N = 3$, $\theta_2 = 0^\circ$ (‘Peaks’ waveform) of (a) the excitation rate at 80 Pa obtained from the PIC simulation with the sheath edges shown in white, (b) the electric field at 80 Pa obtained from the simulation, (c) the experimentally measured excitation rate at 80 Pa, and (d) the experimentally measured excitation rate at 20 Pa. The applied voltage waveform is shown in (e) and (f) for reference, for $\phi_{tot} = 210$ V. The dashed region in (b) designates the region of high bulk electric field shown in figure 7(a). The powered electrode is situated at $x = 0$, while the grounded electrode is located at $x = 25$ mm.
This transition is caused by the low electronegativity (and collisionality) at 20 Pa and the high electronegativity (and higher collisionality) in combination with specific electron dynamics at 80 Pa. At this high pressure a strong excitation maximum is observed at the collapsing sheath edge close to the grounded electrode (see figure 6(a)), which originates from a strong drift and an ambipolar electric field caused by the high local electronegativity [40, 59, 61, 63, 66, 75, 79]. The high local electronegativity is caused by a unique mechanism induced by the shape of the driving voltage waveform, which causes the sheath at the grounded electrode to be collapsed for most of the fundamental RF period. This does not happen at the powered electrode. Therefore, at the grounded electrode, negative ions can enter the sheath region, since the time-averaged electric field is very small and only weakly repels these ions from this region. Consequently, the local electron density and conductivity are depleted and a strong reversed electric field is generated by the high RF current which occurs during the sheath collapse [69]. This electric field causes an excitation maximum at the grounded electrode which is further analyzed in figure 7.

Figure 7(a) shows the reversed electric field and the presence of a potential well formed near the grounded electrode by the (floating) sheath electric field at the electrode during its sheath collapse and an ambipolar field at the bulk plasma side caused by the local slope of the electron density profile (see figure 7(b)) [59]. This peak in the electron density near the grounded sheath edge is generated near the time of sheath collapse (around 12–17 ns) and decays slowly throughout the RF period, as there is no sheath expansion to repel these electrons (until around 65 ns). The peak in electron density and, by extension, the ambipolar electric field, persists throughout the RF period and appears prominently in the time-averaged electron density shown in figure 7(b). Electrons are accelerated by the reversed electric field and are confined in this potential well. Depending on the energy of the electrons accelerated by the field reversal and those confined in this well, ionization (e.g. CF$_4^+$ generation) or attachment (CF$_3^-$ and F$^-$ generation) proceeds very efficiently, as shown in the marked regions of figure 8. Low energy electrons attach to CF$_4$ molecules more efficiently compared to high energy electrons, due to the differences in the cross-sections (see figure 3). This mechanism leads to strong ionization and a source of negative ions inside the sheath region at the grounded electrode. In this way, an even stronger field reversal is generated due to a further local depletion of the conductivity. These effects are self-amplifying until the plasma stabilizes, making the effect self-sustaining (i.e. a closed loop). Consequently, this geometrically symmetric CCP becomes split into an electropositive (or weakly electronegative) half and a strongly electronegative half, due to the above mechanisms (see figure 7(b)).

Figure 8(a) also shows the presence of secondary electrons, which are accelerated in the sheath regions. However, they do not affect the ionization and attachment rates considerably (see figures 8(c) and (d)). Their contribution to the excitation also appears to be negligible in comparison to other power-coupling mechanisms (see figure 6).

The spatio-temporal excitation and electric field plots at $\theta_2 = 180^\circ$ (see figure 9) mirror those at $\theta_2 = 0^\circ$. The simulated excitation and electric field are exact mirrors of the $\theta_2 = 0^\circ$ simulation results, as there is no geometric asymmetry there. The experimental PROES plots are affected by the geometric asymmetry in the experiment, but still closely mirror one another. Here, the region close to the powered electrode is electronegative, while the region close to the grounded electrode is electropositive (i.e. weakly electronegative), according to the simulation. An intermediate regime is found at $\theta_2 = 90^\circ$ (see figure 10), where the applied waveform utilizes a non-optimized slope asymmetry effect.

Several heating mode transitions can be observed as a function of $\theta_2$ or pressure. Specifically, a clear transition from the $\alpha$-heating mode to the drift-ambipolar mode occurs between 20 and 80 Pa for fixed harmonics’ phases and voltage amplitudes (see figures 6, 9, and 10), with the drift-ambipolar mode being favored at higher pressures due to the higher electronegativity and higher collisionality at higher pressures.

Figure 11 demonstrates that adding higher harmonics enhances the sheath expansion heating relative to the
Figure 8. Spatio-temporal plots for 80 Pa, $\theta_2 = 0^\circ$ (‘Peaks’ waveform, $N = 3$, $\phi_{pe} = 210$ V) of (a) mean electron energy, (b) electron density, (c) rate of CF$_3^+$ creation, and (d) rate of electron attachment (i.e. CF$_3$ and F$^-$ creation), as obtained from the simulation.

Figure 9. Spatio-temporal plots for $\theta_1 = 180^\circ$ (‘Valleys’ waveform, $N = 3$, $\phi_{pe} = 210$ V) of (a) the excitation rate at 80 Pa obtained from the simulation with the sheath edges shown in white, (b) the electric field at 80 Pa obtained from the simulation, (c) the experimentally measured excitation rate at 80 Pa, and (d) the experimentally measured excitation rate at 20 Pa. The applied voltage waveform is shown in (e) and (f) for reference.
drift-ambipolar heating. This is due to an increase of the driving waveform’s slope during sheath expansion, which increases the effectiveness of $\alpha$-mode heating. For $\theta_2 = 270^\circ$, this leads to more spatially symmetric excitation dynamics for $N = 3$, since the sheath expansion heating at the powered electrode is enhanced relative to the heating at the grounded electrode at about 28 ns. In terms of the symmetry parameter from equation (2), $\varepsilon$ is less than unity for $N = 2$ and $\varepsilon$ is approximately unity for $N = 3$ at $\theta_2 = 270^\circ$. Thus, we find a negative DC self-bias for two harmonics at $\theta_2 = 270^\circ$, and almost no bias at the same phase for $N = 3$ (see figure 5). The strongly negative bias for $N = 2$ at this phase is caused by the SAE, although its effect is reversed compared to electronegative gases due to the presence of the drift-ambipolar heating mode. In electronegative gases such as argon, positive DC self-biases are often observed for this phase [49–52].

### 4.2. Slope asymmetry

The sawtooth waveforms used here (see figure 2(c)) are realized with the fixed phases and amplitudes defined in section 2; these waveforms consist of three consecutive harmonics of $f = 13.56$ MHz, each with an amplitude according to equation (5). The amplitudes and phases of the sawtooth up waveform for $N = 3$ are: $\phi_1 = 138^\circ$, $\phi_2 = 69^\circ$, $\phi_3 = 46^\circ$, $\theta_1 = 0^\circ$, $\theta_2 = 270^\circ$, and $\theta_3 = 180^\circ$. The sawtooth up waveform yields a fast sheath expansion at the powered electrode as a result of the fast transition from its maximum positive applied voltage to its maximum negative applied voltage, and a fast sheath contraction at the grounded electrode. Conversely, the sawtooth down waveform yields a fast expansion of the grounded sheath as the fast transition occurs from the maximum negative voltage to the maximum positive voltage. The $N = 3$ sawtooth down waveform has the same amplitudes and phases as listed above, with the exception that $\theta_2 = 90^\circ$.

The experimentally obtained DC self-bias ($\eta$) for the sawtooth waveforms is plotted as a function of pressure in figure 12. A significant geometric asymmetry is present, especially at lower pressures ($p \leq 30$ Pa), which prevents comparison of our experimental results to those of the PIC simulations. The bias changes drastically as a function of pressure as a result of the SAE and the geometric asymmetry of the discharge. No AAE can be present due to the identical global extrema in the driving voltage waveform. For the sawtooth down waveform, the sign of the self-bias changes as the pressure increases. In a geometrically symmetric reactor, this would also happen for the sawtooth up waveform. This reversal of the discharge asymmetry as a function of pressure is caused by a transition from the $\alpha$-heating mode to the drift-ambipolar heating mode induced by increasing the pressure.
and thus increasing the electronegativity. Above 50 Pa, the self-bias stays approximately constant as a function of pressure after this mode transition. This is expected to be highly relevant for applications, as it completely reverses the role of the two electrodes with regards to the EAE. For example, a negative DC self-bias voltage corresponds to enhanced excitation at the grounded side, whereas, in electropositive plasmas, it corresponds to enhanced excitation at the powered side.

The sawtooth down waveform causes the grounded sheath to expand quickly and the sheath at the powered electrode to expand slowly, while for the sawtooth up waveform the situation is reversed. At 20 Pa, the discharge operates in the \( \alpha \)-heating mode (see figures 13(a) and (b)). At this low pressure, the discharge is geometrically asymmetric. This results in an increase of the excitation rate at the powered electrode relative to that at the grounded electrode. For the sawtooth down waveform, the spatio-temporal excitation rate at the grounded side during the grounded sheath expansion is more visible compared to that measured for a sawtooth up waveform, as the grounded sheath expands very quickly once per fundamental RF period. Due to the geometric asymmetry of the reactor, the density in the powered sheath is still higher than that in the grounded sheath, i.e. \( \bar{n}_{sp} > \bar{n}_{sg} \). Thus, according to equation (2), the symmetry parameter \( \varepsilon \) is relatively high for this situation, though it is still less than unity due to the geometric asymmetry. The self-bias is then weakly negative at low pressures, according to equation (1).

At higher pressures (50 Pa and 80 Pa, see figures 13(c) and (d) and figures (e)–(f), respectively), the discharge operates in the drift-ambipolar heating mode and there is strong excitation at the powered/grounded electrode for the sawtooth up/down waveform, respectively, where the sheath collapses quickly once per fundamental RF period. This is caused by a mechanism similar to that described in section 4.1. The high negative-ion density leads to a local depletion of the electron density and a strong electric-field reversal at the edge of the rapidly collapsing sheath. The self-amplifying mechanism described before is only effective at one electrode for sawtooth waveforms, where electrons are accelerated towards the electrode (i.e. towards the potential well) and not away from it (and its corresponding sheath). In combination with a reactor with better geometric symmetry, this leads to \( \bar{n}_{sp} \gg \bar{n}_{sg} \) for the sawtooth down waveform, where \( \varepsilon > 1 \) and a positive bias is generated, and \( \bar{n}_{sp} < \bar{n}_{sg} \) for the sawtooth up waveform, where \( \varepsilon < 1 \) and a negative bias is generated. In conclusion, the
change of the DC self-bias and the reversal of the discharge symmetry as a function of pressure for the sawtooth waveforms can be explained by a transition to an electron heating mode characteristic of an electronegative plasma, which is induced by increasing the pressure.

5. Conclusions

The electron power absorption and excitation dynamics in capacitive CF₄ discharges driven by tailored voltage waveforms were investigated experimentally and via numerical simulations, with good qualitative agreement between the two. The discharge pressure, the number of harmonics, and the harmonics’ phases were varied systematically. At high pressures the discharge was found to operate in the drift-ambipolar heating mode, while at low pressures the α-heating mode was dominant. Mode transitions between these two modes were induced by changing the pressure, the harmonics’ phases, and the total number of harmonics.

The presence of the drift-ambipolar mode was found to lead to unique spatio-temporal excitation/ionization dynamics. Depending on the choice of the harmonics’ phases, i.e. the shape of the applied voltage waveform, one strong excitation/ionization maximum per fundamental RF period can be generated at the collapsing sheath edge adjacent to only one electrode. This is due to the extended period where the sheath is

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**Figure 13.** Experimentally measured spatio-temporal excitation rate for sawtooth waveforms \( N = 3, \phi_{av} = 253 \text{ V} \) at ((a)-(b)) 20 Pa, ((c)-(d)) 50 Pa, and ((e)-(f)) 80 Pa. The left column contains the sawtooth down \( \theta_2 = 90^\circ, \theta_3 = 180^\circ \) results, while the right column shows the sawtooth up \( \theta_2 = 270^\circ, \theta_3 = 180^\circ \) results. The applied voltage waveforms are shown in (g) and (h) for reference.
fully collapsed at this electrode in combination with a strong electric-field reversal that accelerates negatively charged particles towards this electrode. Therefore, negative ions can move into this sheath region and locally deplete the electron density and conductivity. This enhances the electric-field reversal at times of high RF current. Moreover, a potential well is formed at this electrode during sheath collapse by the electric field of the (floating) collapsed sheath and the ambipolar electric field in the bulk plasma. Electrons are accelerated by the reversed field toward this well and are confined efficiently in it, leading to an increase in the local attachment rate and the formation of negative ions leading to an increased negative-ion density in the sheath region only at one electrode. This depletes the local conductivity further, increasing the field reversal strength. These mechanisms lead to a self-amplification of the field reversal. In this way, the discharge becomes divided into an electropositive half at one electrode and an electronegative half at the other electrode.

The generation of a DC self-bias via the EAE was found to be strongly affected by the electron heating mode. This was particularly true for sawtooth waveforms, where only the slope asymmetry effect (SAE) causes an electrical generation of a DC self-bias. For such waveforms, the sign of the DC self-bias can be reversed by switching from the $\alpha$-heating mode to the drift-ambipolar heating mode by increasing the pressure due to strongly different excitation/ionization dynamics. Thus, the discharge asymmetry is reversed in electronegative CF$_4$ plasmas operated by sawtooth waveforms in the drift-ambipolar heating mode compared to electropositive plasmas operated in the $\alpha$-heating mode (e.g. CF$_4$ at low pressures and argon at all pressures), due to the unique electron power absorption dynamics induced by voltage waveform tailoring.

These findings are expected to have extremely important consequences for a variety of radio frequency plasma applications, for which CF$_4$ or other electronegative gases are typically used, as the DC self-bias and excitation/ionization dynamics strongly influence the formation of process relevant flux-energy distributions of all particle species, including electrons, ions, and neutrals.

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